



FIG. 2. Time-of-flight (TOF) neutron-diffraction pattern for cubic KCN III with the Maxwellian background mathematically removed. The solid line shows the result of simultaneously fitting all of the peaks using the variable intensity fit as described in Sec. III of the text. The fit is not extended to the (100) peak at the extreme right end of the pattern because of a frame overlap problem which caused the background to rise slightly here. The calculated position of the (100) peak is shown by a vertical arrow. The peaks due to the alumina (Al_2O_3) pressure cell are given with their hexagonal indices.

eters which are the only adjustable parameters affecting the peak positions. α_h and f_h are the peak amplitudes of the KCN peaks and the Al_2O_3 peaks, respectively, and v is an overall intensity factor for Al_2O_3 . The KCN peak amplitudes α_h are treated as variable parameters while the relative amplitudes f_h for Al_2O_3 are held fixed at values determined from a pure Al_2O_3 diffraction pattern. Pb peaks, if present, are treated in the same manner as Al_2O_3 peaks. This allows an accurate subtraction of Al_2O_3 and Pb peaks from the pattern, particularly as these in all cases were very small at the 60° scattering angle. In some regions of the diffraction pattern the intensities obtained from this type of analysis are slightly in error because the assumed shape for the Maxwellian with the three variable parameters is not sufficient to exactly fit the background over the entire spectrum. For the least-squares technique described here, the ratio of χ^2 to the number of degrees of freedom which we shall designate the "goodness of fit" should lie between 0.8 and 1.2 for a perfect statistical fit. In what follows we shall refer to the fit summarized in Eq. (1) as the variable intensity fit.

Since the TOF diffraction method employs a con-

tinuous range of neutron wavelengths (λ), the measured intensities are modified by the thermal neutron spectrum and by a λ^4 multiplication.¹⁶ Relative structure factors were determined from the measured intensities [$I_h^{\text{TOF}} = \alpha_h S_i (\pi/4 \ln 2)^{1/2}$] according to the relation

$$m_h |F_h|^2 \propto I_h^{\text{TOF}} / \lambda^4 I_0(\lambda), \quad (2)$$

where m_h is the multiplicity for the peak with label h in the diffraction pattern, F_h is the structure amplitude including Debye-Waller factors, and $I_0(\lambda)$ characterizes the neutron flux from the reactor. In our case $I_0(\lambda)$ was determined from a measurement of the direct beam transmitted through the pressure cell containing the sample using a detector matched to those used for the 30° and 60° scattering angles, and so $I_0(\lambda)$ should implicitly contain absorption and multiple scattering corrections for both the sample and pressure cell as well as detector efficiency corrections. In fits to the diffraction pattern for well-known cubic materials it was found that the measured $I_0(\lambda)$ predicted structure factors for the diffraction peaks associated with the longer neutron wavelengths which were too low. In order to fit the measured intensities

